| | 50738-65 IWT(m)/EWP(v)/T/IWP(t)/EWP(k)/EWP(b)/EWA(c) Pf-5 TK/JD/IN4 UR/0286/65/000/009/0081/0081 |
|-----|---|
| Á | 50738-65 IWT(m)/EWP(w)/T/WP(t)/LWP(k)/EWP(D)/DD 1070286/65/000/009/0081/0081 CCESSION NR: AP5015325 620.115.82 |
| 1 | THOP: Yermolov, V. A.: Kazakevidi, V. I.; Chukhrov, D. L.; Shlenskiy, V. A. |
| | CITILL A 21 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 |
| 1 . | SOUR E: Byulleten' izobreteniy i tovarnykh znakov, no. 9, 1965, 81 |
| : | TOPIC TAGS: solder, tensile test, test equipment |
| | ABSTRACT: This Author's Cartificate introduces a solder specimen made up of a rod |
| -1 | nical properties of a solder joint and the surface of the rod is an argular groov, of a definite size which is the surface of the rod is a continuous groove through which the solid solder. On the end of the rod is a continuous groove through which the solder flows after heating of the sample. The rod and the sleeve are threaded to- |
| - | solder flows after heating or the sample. |
| | ASSOCIATION: Predprivative gosudarstvennogo komiteta po oboronnov tekhnike SSSR |
| | Card 1/2 |
| | |

| Cimirmon | R: AP5015325 | | المراجع والمعاولات المعادية ا | | - |
|-------------|--------------|--------------------------|--|--------------|---|
| | 28Sep63 | ENCL; | | SUB CODE: IE | |
| NO REF SOV: | 000 | other: | 000 | | |
| PARTE | | া মৰ পায়ৰ চেক্টেইছেছিল। | | | |
| TAKE 3 | | | en e | | |
| | | | | | |
| | | | | | |
| | | | | | 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| | | | | | |
| | | | | | |
| | | | | | |
| | • | ¥. | · | • | |
| | - | • | • | | |
| | | | | | |

KAZAKEVICH, V.M., insh.; KONDRATYUK, A.P., insh.

Operating conditions of coupling transformers with the power system in electric power plants. Elek.sta. 29 no.5:46-47 My '58. (MIRA 12:3)

(Electric power plants) (Electric transformers)

"APPROVED FOR RELEASE: 06/13/2000

CIA-RDP86-00513R000721230005-1

L 01083-67 EWT(m)/EWP(j)/T ZIJP(c) OD/RM
ACC NR: AT6031600 SOURCE CODE: UR/0000/64/000/000/0185/0189

AUTHOR: Yerofeyev, B. V.; Shlyk, V. G.; Kazakevich, V. S.

321 1:/:

ORG: none

TITLE: Similarity of the initiating action of salts of metals capable of assuming several valences, in autocatalytic oxidation and polymerization. 1. Comparison of the efficiency of carboxylates differing in the hydrocarbon chain length

SOURCE: Geterogenmye reaktsii i reaktsionnaya sposobnost! (Heterogeneous reactions and reactivity). Minsk, lzd-vo Wyshaya shkolk, 1964, 185-189

TOPIC TAGS: chemical initiation, polymerization rate, autocatalytic oxidation, cobalt, carboxylate, manganese stearste, lead, stearste, styrene, tetralin hydroperoxide, autocatalysis, chemical valence

ABSTRACT: A study has been made of the effect of carboxylates of metals capable of assuming several valences on the polymerization rate of styrens in the presence of tetralin hydroperoxide. The experiments were conducted with several cobalt carboxylates (formiate, acetate, butyrate, caprylate, and stearate), and with manganese or bead stearates. The dependence of the polymerization rate on the hydroperoxide

Card 1/2

L 01083-67 ACC NR: AT6031600

and carboxylate concentration was studied. It was shown that the polymerization rate of styrene, in the presence of hydroperoxide—carboxylate systems, depends both on the nature of the metal and of the anion. The initiating efficiency of the carboxylates increased with the hydrocarbon chain length, that of the metals in creased in the order: cobalt < manganese < lead. Thus, the initiating action of the carboxylates considered in polymerization is similar to that in autocatalytic oxidation. A scheme is proposed which explains the initiating action of carboxylates as a result of the substitution of hydroperoxide for acid radicals. Orig. art. has: 3 figures.

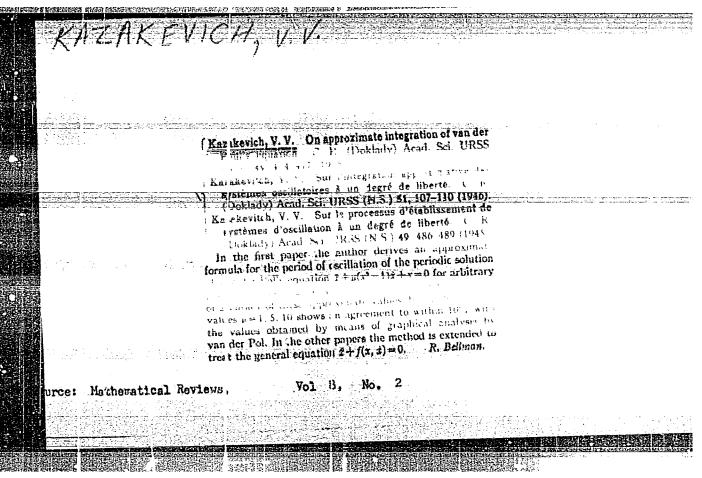
SUB CODE: 07/ SUBM DATE: 12Dec 64/ ORIG REF: 007

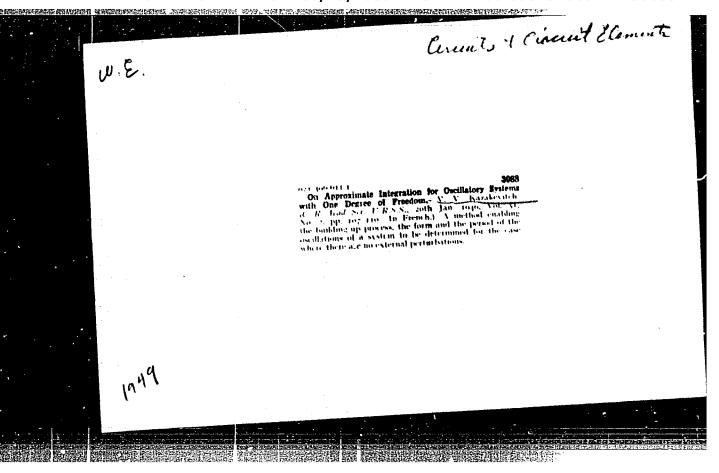
Card 2/2 MJ

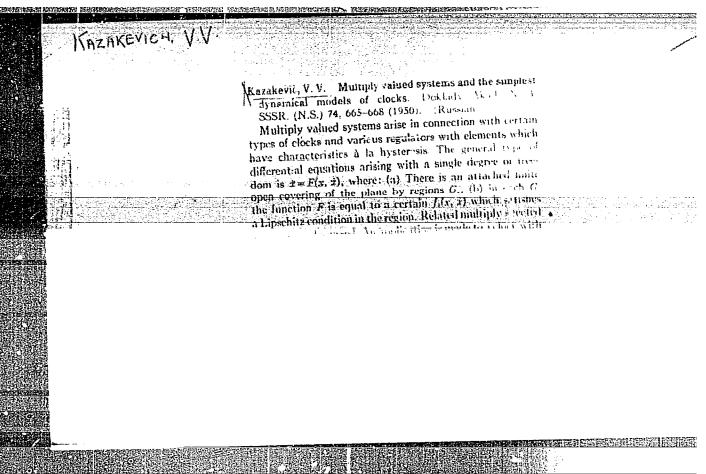
GLADKIKH, S.A.; KHACHATURYAN, S.A.; KAZAKEVICH, V.V., doktor tekhn. nauk, prof., retsenzent; BODNER, V.A., doktor tekhn. nauk, prof., retsenzent; DANILOV, L.N., inzh., red.; DANILIN, L.N., red.izd-va; TIMOFEYEVA, N.V., tekhn. red.

[Preventing and eliminating vibrations in pumping units]
Preduprezhdenie i ustranenie kolebanii nagnetatel'nykh ustanovek. Moskva, Izd-vo "Mashinostroenie," 1964. 274 p.

(MIRA 17:4)







| H BETHERE THE PERSON OF THE PE | 在中心的主义的 中的主义的特殊的 医克尔特氏 经公司的 医多种性 医皮肤 | LA TOLYAN |
|--|--|--|
| KAZAKEVICH, V. V. | | |
| | DBSR/Mat of auto Coulomb ment. after r | A/Ha antri cape cape cape cape cape cape cape cape |
| | R/Mathematic automatic lomb fric Submiter revisi | thematical bution thements), at 1 Tele applies applies applies applies applies applies to the construction and construction a |
| | · | l oct BC B a |
| | | cts multi- constr of |
| | | hematics - Speed Reguintion to the Theory ontion to the Theory onents)," v. v. Kazakev pents)," v. v. Kazakev of applies the theory of ed by him ("Dok Ak Named by to analysis of constructs multi-leaf and conducts quant in of the constr of multi-leaf |
| | Regarda Negata | cmatics - Speed Regulators Clocks, Escapements (clocks, Clocks, Cl |
| | negurators ntd) system in the cuent in the sens h9; resubmitted | Escapements Escapements Y of Trip Regul kevich " TI, No 1, pp 4] Of manifold sy Nauk SSSR" Vol of processes in esf phase surfa investigation. multi-leaf phas |
| | | Jan, nts Regulat Regulat pp 41-6 pp 41-6 pld syste N' vol 11 ses in es surface stion. f phase |
| | | Jan/Feb pulators gulators systems, vol ixxiv in escap rface of on. Give hase surf |
| | E C S | HI THE THE STATE OF A CO. |
| | 187T35 | 251 187135 |
| | Mary de l'arient de final a la communication de la communication d | |
| | | Commission of the commission o |

KAZAKEUICH, U.U.
SOLODOVNIKOV, V.V.; professor, doktor tekhnicheskikh nauk, redaktor; AYZERMAN, M.A., doktor tekhnicheskikh nauk; BASHKIROV, D.A., kandidat tekhnicherkikh nauk; BROMBERG, P.V., kandidat tekhnicheskikh nauk; VORONOV, A.A., kandidat tekhnicheskikh nauk, dotsent: GOL'IFARB, L.S., doktor tekhnicheskikh nauk, professor; KAZAKEVICH, V.V., doktor tekhnicheskikh nauk; KRASOVSKIY, A.A., kandiuat tommicheskikh nauk, dotsent; LERNER, A.Ya., kandidat tekhnicheskikh nauk; LETOV, A.M., doktor fiziko-matematicheskikh nauk; professor; MATVEYEV, P.S., inzhener; MIKHAYLOV, F.A., kandidat tekhnicheskikh nauk; PETROV, B.N.; PETROV, V.V., kandidat tekhnicheskikh nauk; POSPELOV, G.S., kandidat tekhnicheskikh nauk, dotsent; TOPCHNYEV, Yu.I., inzhener; ULANOV, G.M., kandidat tekhnicheskikh nauk; KHRAMOY, A.V., kandidat tekhnicheskikh nauk; TSYPKIN, Ya.Z. doktor tekhnicheskikh nauk, professor; LOSSITEVSKIY, V.L., doktor tekhnicheskikh nauk, professor, retsenzent; TIKHONOV, A.Ya., tekhnicheskiy redaktor

[Fundamentals of automatic control; theory] Osnovy avtomaticheskogo regulirovaniia; teoriia. Moskva, Gos. nauchno-tekhn. izd-vo mashino-(MLRA 8:2) stroit. lit-ry, 1954. 1116 p.

1. Chlen-korrespondent AN SSSR (for Petrov, B.N.) (Automatic control)

KAZAKEVICH, V.V. (Moskva).

Use of throttle devices for measuring fluid consumption at low Reynolds numbers. Izv. AN SSSR. Otd. tekh. nauk. no.12:125-128 D 155. (MIRA 9:3)

KAZAKEVICH, V.V.

SUBJECT

USSR/WATHEMATICS/Differential equations CARD 1/1 PG - 150 KAZAKEVIČ V.V.

AUTHOR TITLE

PERIODICAL

On irrelation between phase planes of Raileigh's equation and

van-der-Pel's aquation.

Doklady Akad. Nauk, 107. 521-523 (1956)

reviewed 7/1956

As is well known, by y = x and F(z) = df(z)/dz the Raileigh's differential equation $\ddot{y} - hf(\dot{y}) + y = 0$ can be transformed to the van-der-Pol's equation z - MF(z) z + z = 0. After a short general consideration the author shows by the example $f(y) = y - y^3$ that the corresponding phase planes show no visible coincidence; e.g. the limit cycles have a very different form.

KAZAKEVICH. V.V

Characteristics of the excitation of vibrations in clocks. Dokl.AN SSSR 107 no.5:653-655 Ap '56. (NIRA 9:8)

1. Predstavleno akademikom N.W. Bogolyubovym. (Clocks and watches--Vibration)

AUTHOR:

Kazakevich, V. V.

20-4-12/60

TITLE:

On Surging in Compressors (O pompazhe v kompressorakh).

PERIODICAL:

Doklady Akademii Nauk SSSR, 1957, Vol. 115, Nr 4, pp. 677-680

(USSR)

ABSTRACT:

At first a short report is given on 6 relevant earlier works. The present paper investigates the character of the surgingoscillations and a method for their suppression. The system examined here contains a ventilator, a sucking pipe and a pressing pipe on whose outlet is a regulating resistance in form of a throttle. The author assumes the following: 1) The complicated distributed acoustic system can be replaced by a system with one degree of freedom. 2) The changes pressure in the oscillations are small. Then the motions in the system can be described by a system of two first order differential equations:

 $dQ_0/dt = (1/L_a)[F(Q_0)-p]$, $dp/dt = (1/C_a)[Q_0 - \phi_1(p)]$

In this connection $\varphi_1(p)$ signifies the increase in the function: $\varphi(Q_R)$; Ca- the acoustic mobility of the system, L_B-the acoustic mass, and $F(Q_0)=\pi_1(Q_0)$ -p₀ applies. By eliminating the time from these equations the differential equation of the integral curves is obtained; $dp/dQ_0 = ((Q_0 - \phi_1(p))/(F(Q_0)-p))L_a/C_a$. After some

Card 1/2

transformations expressions for the condition of the static prin-

SUBMITTED:

February 2, 1957

AVAILABLE:

Library of tongress

CarAPPROVED FOR RELEASE: 06/13/2000

CIA-RDP86-00513R000721230005-1"

前是"最高的现在分词在全面在了面上,我们就是不过有去。"他是一个是是一个的话的是一个一个的话的。 ———————————————————————————————

KAZAKEVICH, V.V.

AUTHOR:

Rusevich, I. M.

103-2-9/9

TITLE:

Conference on Automatic Control and Computation Engineering (Soveshchaniye po avtomaticheskomu upravleniyu i vychislitelinoy tekhnike)

PERIODICAL:

Avtomatika i Telemekhanika, 1958, Vol. 19, Nr 2, pp. 191-194 (USSR)

ABSTRACT:

From March 5 - 8, 1957 the conference on automation and computation engineering organized by the All Union Scientific Engineering and Technical Society for Apparatus Building took place. 900 delegates from the Institute of the AN USSR as well as of the AN of the Unions' Republics, universities, research institutes, designing offices and laboratories of the various ministries and authorities took part in it. 40 lectures were held. The opening speech was delivered by M. Ye. Rakovskiy. The president of the organization committee of this conference V. V. Solodovnikov (Central Scientific Research Institute for Complex Automation = TenIIKA) announced the tasks as well as the program of the conference. In the

Card 1/6

Conference on Automatic Control and Computation Engineering

second part of his speech he defined the subject as well as the characteristics of the content of technical cybernetics. A. A. Lypunov indicated the role and the importance of cybernetics as scientific basis of a complex automation of production. The following lectures were held on the theory and the foundations of construction of control computors: V. V. Kazakevich spoke on "Principles and circuits of optimum operation control methods". In a common lecture V. V. Solodovniko, A. M. Batkov, A. A. Bredis and P. S. Matveyev (TsNIIKA) dealt with the "Present Stage of the Theory of Optimum Dynamic Systems Subjected to Arbitrary Effects". L. T. Kuzin showed the use of the Z-transformation apparatus for the analysis and synthesis of the automation systems with numerical computation devices. A. M. Batkov spoke on the new way of using modelling electronic plants (electronic simulation) for the determination of the basic and statistical characteristics the correlation function and the dispersion of a non-standardized arbitrary magnitude at the output of the automation system according to given characteristics of arbitrary effects at the input. Yu. A. Shreyder spoke on the principles of construction of so-called "self-informing" control apparatus, the

Card 2/6

Conference on Automatic Control and Computation Engineering

basic property of which is the capability to find the optimum way of control by means of accumulated experiences in operation. - V. I. Dikushin, Member of the Academy, (Scientific Research and Experimental Institute for Machining Tools) spoke on the construction of systems for a preset control of machine tools. The lecture of E. Z. Lyubimskiy, S. S. Kamynin and V. S. Shtarkman (Institute for Mathematics imeni Steklov AN USSR) dealt with optimum information coding in automation and multistep automation schemes for production processes. M. P. Shura-Bura (Institute for Mathematics imeni Steklov AN USSR) spoke on the possibility of using the means of computation engineering for a transformation of any informations including those of automatic translation from one language into the other. N. V. Korol'kov, Ye. I. Mamonov and Yu. I. Sharapov spoke on the achievements in the field of quick, reliable, economical and small computor elements. On the utilization of these elements in the circuits of computors spoke V. A. Zimin and L. I. Gutenmakher. - V. I. Ryzhov, N. V. Trubnikov and A. K. Zavolokin, as well as Ye. M. Baskakov spoke on the input and output devices of computors. Yu. S.

Card 3/6

Conference on Automatic Control and Computation Engineering

Val'denberg held a lecture on a specialized mathematical machine of continuous operation for the solution of integral equations of Fredholm and Volterra's first and second type, as they often occur in control problems. - Yu. V. Novikov (IAT AH USSR) spoke on the new computor created in the IAT AN USSR (magnetic correlograph) for the automatic computation of correlation functions. - I. M. Vitenberg spoke on the modelling electronic apparatus for the automatic finding of a solution for a problem with a given system of equations. - F. V. Mayorov and Ye. P. Zhidkov spoke on the mathematical foundations of numerical differential analyzers (TsDa) as well as on their use as control apparatus. - L. I. Gutenmakher spoke on the prospects of using information- and statistical machines of new design for control systems.

AVAILABLE:

Library of Congress

Card 4/E

Conference on Automatic Control and Computation Engineering

The conference took place in Moscow from March 5 - 8, 1957. A number of lectures dealt with examples from the field of application of computation apparatus for the control of real production objects Yu. Ye. Yefroymovich (Central Laboratory for Automation), V. Yu. Kaganov (Central Laboratory for Automation, A. B Chelyustkin (IAT AS USSR) and P. N. Kopay-Gora spoke on the use of computation apparatus for the control of basic objects in matallurgy (furnaces, are furnaces, rolling mills). D. T. Vasil'yev and L. N. Fitsner spoke on computators for the determination of the most suitable sequence of cuts in metalworking industry. Up to 20 different quantities determining the sequence of cuts can be introduced into the

Cerd 5/6

Conference on Automatic Control and Computation Engineering

machine and when some of these magnitudes are given the demanded optimum parameter can be computed within 2 - 3 minutes. Ya. A. Khetagurov reported on a numerical system for the control of a machine tool. - The conference regards it necessary to organize special groups within the TaNIIKA (Central Scientific Research Institute for Complex Automation), the NII and KB (Scientific Research Institute and Construction Bureau), at the ministries as well as within the organization of the AS USSR. These groups should be concerned with the problems of technical cybernetics. It was decided to have organized an All-Union Conference for Cybernetics by the All-Union Scientific Engineering and Technical Society for Apparatus Building in collaboration with the AS USSR.

AVAILABLE:

Library of Congress

1. Automation-Conference

Card 6/5

USCOMM-DC-54858

PHASE I BOOK EXPLOITATION

sov/3486

Kazakevich, V. V.

Avtokolebaniya (pompazh) v ventilyatorakh i kompressorakh (Self-excited Oscillations /Pulsation/ in Ventilators and Compressors) Moscow, Mashgiz, 1959. 191 p. 6,000 copies printed.

Sponsoring Agency: Nauchno-tekhnicheskoye obshchestvo priborostroitel'noy promyshlennosti.

Tech. Ed.: S. M. Lazarev.

PURPOSE: This monograph may be used by engineers and technicians, designers and application engineers, scientific workers, and students of advanced courses in the appropriate fields in schools of higher technical education.

COVERAGE: The theory developed in this book permits one to explain basic phenomena occurring in self-excited oscillations, shows the causes for differences in the character of oscillations in various types of fans, and evaluates the effect of various factors on the domain of oscillating regimes. This

Card 1/6

APRROVED FOR BELEASE \$ 06/18/2000 CIA-RDP865005138000721230005-1"

theory enables one to predict new phenomena. It shows in particular that oscillations may take place not only in regimes corresponding to ascending branches of the characteristic curves, but also in regimes corresponding to the descending branches, which up till now were considered stable. The book also shows a method of constructing (directly from the fan and system characteristics) curves which characterize the oscillations. The new theory also makes it possible to eliminate oscillations by introducing a regulating system with feedback, which affects the position of the throttle and distributor. There are 13 references: 11 Soviet, 1 English, and 1 German.

TABLE OF CONTENTS:

| Introduction | 5 |
|---|----------------------------|
| Ch. I. Equations of Motion of a Small-discharge Compressor and Their Analysis Derivation of the equations of motion Reduction of a system of two differential equations of the first order to one equation of the second order Condition for self-excitation of oscillations and their frequencies Effect of external conditions on oscillating characteristics | 12 12 16 20 25 |

Card 2/6

| Self-excited Oscillations (Cont.) | sov/3486 | |
|---|---------------------|--------------|
| Behavior of a system "on a small scale" (domains and static stability) | , | 2 |
| Analytical determination of the amplitude and pe self-excited oscillations | , | 5 |
| manufaction of the equation of motion to Ray | | 9 |
| Investigation of a system "on a large scale." Scitation of oscillations | | .5 8 |
| Domains of stability and instability Unstable operation on the descending branches of | f the compressor | |
| characteristic More complex cases of oscillation | l l | '0 '4 |
| Ch. II. Method of Integrating the Oscillation Equa | ation Directly From |) |
| the Fan and System Characteristics | • | 33 33 |
| Basis of the method Determining the period of oscillations | | 39 92 |
| Physical meaning of the phase plane Investigation of oscillation in a specific syst | • |) |
| The effect on the character of oscillation brown change in position of the operating point on the | gnt about by a | 93 |
| Card 3/6 | | |

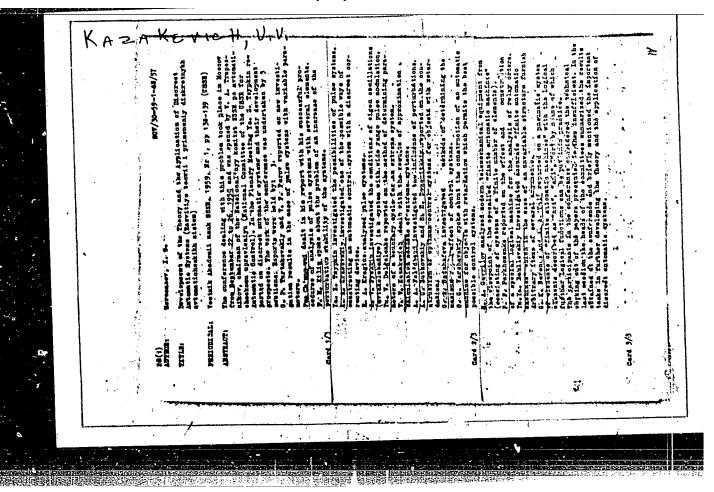
| Self-excited Oscillations (Cont.) Sov/3486 | |
|--|-----|
| Determination of the period of oscillations | 101 |
| Effect of a change in the geometrical dimensions of the system | 102 |
| Construction of curves showing pressure and discharge as | 117 |
| functions of time More complex cases where pumping arises | 125 |
| Investigation of motions in a system where several points of intersection between compressor and network exist | 123 |
| Ch. III. Oscillations in Systems With a Large-discharge Compressor | 125 |
| Derivation of equations of motion | 125 |
| Amplitude of the equations of motion | 129 |
| Conditions of soft and hard excitation of oscillations according | 131 |
| Oscillation in systems containing a throttling valve in the succi | 133 |
| line | 133 |
| Derivation of equations of motion | 136 |
| Construction of the compressor characteristic | 140 |
| Phase plane of the system Derivation of the stability condition | 142 |
| Card 4/6 | |

| Self-excited Oscillations (Cont.) | sov/3486 |
|---|--|
| Stability of a system in which the air at positions other than at the ends of | the line |
| Investigation of motion in systems in and discontinuous compressor characters. Comparison of theoretical and experimen | the presence of hysteresis |
| Determination of the frequency of oscil the geometrical dimensions of the systematical dimensions dimensions dimensions dimensions dimensions discussed the systematical discussed discussed discussed discussed discussed discussed dis | Liations as a lunction of |
| revolutions per minute Determination of the limit of the doma: | 161 |
| Construction of the phase plane Experimental investigations performed especially for checking theory | on axial compressors, 165 174 |
| Methods of influencing oscillations Regulation of the discharge throttle a Regulation of the discharge throttle a Regulation of the distributor accordin | coording to p.d 177 coording to Qo 180 |
| Measurements required in conducting ex | periments 181 |

Card 5/6

APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000721230005-1"

| Self-excited Oscillations (Cont.) | sov/3486 | |
|---|-----------------|-----------------|
| Conclusions | | 182 |
| Appendix. Mechanical Model of a System Repr | resenting a Fan | 184 |
| Bibliography | | 189 |
| AVAILABLE: Library of Congress | | |
| | | |
| | | |
| | | |
| | | |
| Card 6/6 | AC 5- | :/fal .27-60 |
| card o/o | | |
| | | |
| | | |
| | * | |



APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000721230005-1"

KAZAKEVICH, V.V.

Theory of escapement mechanisms with consideration of multiple-valued characteristics. Avtom. upr. i vych. tekh. no.2:167-220 '59.

(MIRA 13:2)

(Time measurements)

KAZAKEVICH, V.V.; OSTROVSKIY, G.M.

Drying friction in a servomotor as a cause of self-scillations in control units. Avtom. upr. i vych. tekh. no.2:296-317 159.

(MIRA 13:2)

(Servomechanisms)

SOV/24-59-4-15/33

AUTHORS: Bodner, V.A. and Kazakevich, V.V. (Moscow)

TITLE: Stability of Compressors as Non-linear Elements in

Extended Systems

出现现在的情况,我们就是我们的知识的知识的是我们就是我们的一个,我们可以不是一个,我们也没有什么,我们就是这一个,我们就是这个人的,我们就是这个人的,我们就是

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh

nauk, Energetika i avtomatika, 1959, Nr 4, pp 116-125 (USSR)

ABSTRACT: The compressor is one supplying compressed air to remote

points through narrow pipes; the compressor is controlled by the pressure prevailing at a fairly distant point. The equations of motion (taken from Ref 1) are (1.1), where u, p and O are, respectively, the speed, pressure and density, d is the diameter of the pipe,

 α and m are coefficients representing viscous resistance and γ is the ratio of the specific heats. It is assumed that the pipe (Figure 1) is loaded at the ends by acoustic impedances $^{\rm Z}_{\rm 1}$ and $^{\rm Z}_{\rm 2}$; the boundary

by acoustic impedances z_1 and z_2 ; the boundary conditions are then (1.2), where p_1 and p_2 are the

total pressures at the input and the output, respectively;

pol and po2 are the constant components of those

Card 1/5

Sov/24-59-4-15/33
Stability of Compressors as Non-linear Elements in Extended Systems pressures; Q_1 and Q_2 are flows (in volume terms) are excess flows (again in volume terms). q_1 The equations are linearized (Ref 1) as (1.3 and (1.4), and with the symbols defined at the top of p 117; the boundary conditions are put as (1.5). It is assumed that and h₂₁ are constant for the purposes of examining the stability, though this is not so in unstable modes (variation in $\partial F/\partial Q_2$ is used as a test for instability). In the second section, the equations are solved using the form given by Eqs (2.1) and (2.2), which with (1.3) and (1.4) give (2.3) for the input pipe and (2.4) for the output pipe; the corresponding solutions are (2.5) and and Z22 are the wave impedances of (2.6), where 211 the pipes. Eq (2.7) gives the constants A and B; this system has a solution only if (2.8) is complied with. The two equations derived from (2.8) are (2.9).

Card 2/5

SOV/24-59-4-15/33 Stability of Compressors as Non-linear Elements in Extended Systems Then (2.8) is put as (2.10), with $E_{11} = -E_{12}$. In section 3, the compressor is assumed to be connected to a pipe terminated by an impedance Z, , with an impedance Z₁ at the input by the compressor (here l_1 = 0). The substitutions at the top of p 119 are then made, to give (3.1), which then splits up into Eqs (3.2) and (3.3); these equations show that the natural frequencies of the system depend only on the pipe and terminating impedance and that there are two series of frequencies given by Eq (3.4). First, the roots corresponding to the + sign are considered, with $|Z_2| \ll Z_{22}$; we then have Eq (3.5), which leads to a $|\mathbf{Z}_2| \gg \mathbf{Z}_{22}$ and we have contradiction. Therefore, Eq (3.6). Then the -sign is taken, again with $z_2 < z_{22}$; $\langle z_2 \rangle \gg z_{22}$ gives this gives Eq (3.7). The case Eq (3.8). This argument shows that the minus sign must Card 3/5

SOV/24-59-4-15/33 Stability of Compressors as Non-linear Elements in Extended Systems

be taken and Eq (3.9) gives the frequencies.

The subsequent analysis deals with the stability limits, which are given by Eq (3.13); the case $\psi = 0$ is considered in detail. Here, Eq (3.12) becomes (3.15), which implies Eqs (3.16) and (3.17); these define, respectively, the regions of dynamic and static stability. Figure 2 illustrates this. Figure 3 shows lines of constant decrement.

The next section deals with the effects of radiation from the open end of the pipe, assumed fitted with an infinite flange. Figure 4 illustrates the results in general terms. Eq (3.19) onwards deal with the effects of an impedance Z_1 connected at the compressor end; at no point can the system then become absolutely unstable. The system is, respectively, least and most stable when the two equations for R_1 apply. The final two sections deal with other special cases, the significance of which

Card 4/5

16(1) AUTHOR:

Kazakevich, V. V.

SOY/20-126-2-17/64

TIPLE:

On the Monotonic Stability of Invariant Points (O monotonnoy ustoychivosti invariantnykh tochek)

PERIODICAL:

Doklady Akademii nauk SSSR, 1959, Vol 126, Nr 2, pp 287-290 (USSR)

ABSTRACT:

The system of equations $\varphi_i(x_1,\ldots,x_n)=f_i(x_1^{(1)},\ldots,x_n^{(1)})$, $i=1,\ldots,n$ is assumed to define the unique transformation T, according to which it is possible to pass from point P(x, ..., xn) to point

 $P_1(x_1^{(1)},...,x_n^{(1)}) = P_1=T(P)$. The above-mentioned equations are

assumed to determine the invariant point $P^*(x_1,...,x_n^*)$. The following then holds: $f_1(x_1,...,x_n^*) = \psi_1(x_1^*,...,x_n^*)$. The author determines the monotonic stability with respect to $x_1,x_2,...,x_n(k_n)$.

The condition of monotonic stability is, of course, more rigorous than that of asymptotic stability, and it is also of practical use, for many problems of automatic control are reduced to a point transformation of a straight line into a straight line or, in

Card 1/3

On the Monotonic Stability of Invariant Points

SOV/20-126-2-17/64

general cases, of a space into a space. Especially the problem of the exact determination of periodic motions in a system serving the purpose of automatic control may be reduced to such ϵ transformation, and the application of the criterion of monotonic stability is found to be of use in this case. The author derives the criterion of monotonic stability by basing on the assumption that $\mathbf{f_i}$ and $\mathbf{\phi_i}$ are holomorphic in the neighborhood of the invariant point P. The corresponding calculations are followed step by step. $x_i = x_i^* + a_i$ is put. The condition of monotonic stability demands that $a_p = 0$ (p = k+1, k+2,...,n) holds, which must hold also for all transformations T. Thus, the problem of monotonic stability is reduced to the condition of positivity and definedness of a quadratic form of k variables while at the same time the lastmentioned conditions are satisfied. The invariant point of the initially written down system of n equations with n variables is monotonically stable if the inequalities

Card 2/3

On the Monotonic Stability of Invariant Points

sov/20-126-2-17/64

and the above written down conditions are satisfied. Thus the here investigated monotonic stability requires that several initial conditions ($a_p = 0$) be satisfied, like in the case of the monotonic stability of a system of differential equations. In conclusion, the special cases k = 1 and k = n are investigated. There are 6 references, 5 of which are Soviet.

PRESENTED:

December 31, 1958 by N. N. Bogolyubov, Academician

SUBMITTED:

December 30, 1958

Card 3/3

24 (0)

AUTHOR:

Kazakevich, V. V.

SOV/20-126-3-16/69

TITLE:

On the Process of the Extreme Regulation of Inert Objects in the Presence of Perturbations (O protsesse ekstremal'nogo regulirovaniya inertsionnykh ob"yektov pri nalichii

vozmushcheniy)

PERIODICAL:

Doklady Akademii nauk SSSR, 1959, Vol 126, Nr 3, pp 517-520

(USSR)

ABSTRACT:

In the present paper the inexactitude of regulation caused by the inertia of the objects to be regulated is briefly described, and it is shown that the exactness of regulation depends also on the level of the perturbation. Investigation of the methods of reducing the influence of the inertia of objects and for the attenuation of the influence of perturbations are then given as the subject to be dealt with by the present paper. The investigation is based on an inhomogeneous differential equation of the first order, in which the input- and output quantities x and y of the objects to be regulated as well as their time constant T are put into relation. The solutions given for this differential equation are limited to a range

Card 1/2

of x and y, in which $T \sim$ const. From these solutions the

SAN SALENTANDE TRANSCONTANTANDE AND THE STATE OF THE SECONDARY AND AND SECONDARY SECONDARY SECONDARY AND AND SECONDARY AND ASSESSED AND ASSESSED ASSESSED AND ASSESSED ASSESSEDADAS ASSESSED ASSESSED ASSESSED ASSESSED ASS

On the Process of the Extreme Regulation of Inert Objects in the Presence of Perturbations SOV/20-126-3-16/69

unknown quantities T_i and a_i are calculated. For the case of monotonic oscillations, a similar differential equation is then given and its unknown is determined. On the basis of results hitherto obtained, the process of regulation is then investigated with the help of a diagram (Fig 1). In this connection, the transition process is described with formula (1). The inertialess objects are then briefly investigated, after which the non-monotonic oscillations are dealt with. Two measuring arrangements (Figs 2, 3) for objects of little inertia are then described. In conclusion, determination of the direction of set point displacement by means of these instruments is lealt with in detail. There are 3 figures and 6 references, 4 of which are Soviet.

PRESENTED:

December 31, 1958, by N. N. Bogolyubov, Academician

SUBMITTED:

December 30, 1958

Card 2/2

| | KAZAKEV. ett, K.V. |
|---|--|
| 2 | The presented at the lat fact Congress of the latt Potential of Automatic and 1860, Moscov, 1858. Inthirating, and the latter of the latter o |
| | This presented at the lat latel Congress of the Intil Poderation of Autor, 53 Nurs, 5 |
| • | control, 25 Aur.5 Aut. 5 Aur.5 A |
| | |

| | card 4/4 | | System With Compressed Will like Suppression of Soft-Systliations by Head of Feedbacks | the Second Order Bridger, F.A., J.V. Kazwiseich. St.Dil | 5.0 | With Veriable Parameters Better, A.M. Ceriain Problems of the Theory of Literar Systems With Veriable Fernanciers During Anodes Actions | Potapov, M.D. On the Monstationary Pr | PRIME INTERIOR OF THE ACT OF THE |
|--|-----------|---|---|--|------------------------------------|--|---|---|
| | | | westen of Salf-Greillations by | orange or simple upcames motely systems of Accessing | Ting the Quality of a Control Loss | Theory of Linear Systems With | Properties of Sumpled-Data Systems of the linear Thomas of Control Su | 507/ 577.3 (i.i., 1960 Schnitzen: Making (the boy, Lesier Fryster, p. 1 Fryster, p. 1 |
| ************************************** | #5/75/ata |) | F-12 | 119 419 | System 377 | Vertable 302 | 218 | (Automatic C. 429 p. C. 429 p. C. 429 p. Design of services of |

| Indicativity proposant teril 1 primently distributed avoid the state of the control of the contr | V A- | NV | FIL | 0 | 4 17 | 1/ | | | - | | | 1 | | | | | |
|--|--------------------|--|--|-----------------------------|---|--|---|---|--|--|---|---|---|---|--|------------------------|-------------|
| PRICE I DOR ETPLICATION Dones, 1972 Roders, 1972 Roders | <u> FHZ</u> | HA | LVI | <u>/</u> | الا رح | <u> </u> | • | | | | | | | | | | |
| prisonentys distretryth extonations of the service Attenuted 5,000 copies printed. (a) 1972, 972, 9,000 copies printed. (b) 2502, 972, 9,000 copies printed. (c) 1972, 9,000 copies printed. (c) 1972, 9,000 copies printed. (d) 1972, 9,000 copies printed. (e) 1973, 1974, 1970 codilitate of the strength in termedick is telesublanki. (e) 261 copies, A.A. Fell does, bostor of technical facts of technical Sciences, 15. Formano (Scientific Sources), 15. Formano (Scientific Sourc | ETW & FREE BY COME | Dolgolanko, Yu.V. (LaningTed). Illing: IC TRILY Tystems of Op The sutbor presents his set the regular obtained by the are 2 references, both Sort | Enishevich, Z.I(Noscow). In mailting Confficter The investigation of optima systems of nonlinear differ method of investigation. I | | Bailerskir, It.Is. (Masow). duction Method The author exainss condition of a green to the form of a stense. | optionisting graduate country options fair to sea the process of actomatic sea the process. Some of the sore ing the dispussion of the the fantasations. Personal | specialized functional coar group of papers includes in of the simplest types of se which are developed as rela- | pulse regulators have also pulse regulators froblers digital sprimes. Problers computers for the suturable computers for analog width, radio common of analog width conversions. | of relay control processes the state of the state of the state and of pulse systems with several phenomena in state of the | corraids: The Conference on the Internation Justices both Plans the Title Conference during the first conference during and terhalizes of discussed agos. The press of discussed agos, the press of the first group optimize | purpost: These transactions at other specialists in automat | Editorial Board: N.A. Garrilov Doctor of Technical Sciences A.Ts. Larrer, boctor of Tech G.S. Pappalar, Doctor of Te- Ediances, A.T. Ehrmoy, Cant Doctor of Technical Sciences Oriences; El, of Publishing | Sponsoring Agenty: Akademiya mocheskomu upravleniyu. Instii | Teoriya 1 primereniye diskretnyk (Theory and Application of D: Conference) Hoscov, AN SSS | Monferentelya po voprosem teorii Noscow, 1958 | 724 | |
| Inhebilih sistem, inns of the tell of the street, the | | teing Lacing | westigation of Ecclinoar Processes lising control systems is connected wantial equations. The author appli- here is 1 Sowiet reference. | EXIMALIZING CONTROL SISIEMS | Solution of Tire toglash Equations use and the retired of solution of a seption. There is 1 % | its of studying the effects of rand inag, and examples of eitsting critical independing communications and ob- marious conference papers have also titles and references ancompany mos | order: hard best included in the control hard best included prairies and certain prairies. Her y pulse and digital levices. Her includes the control of the | best included. The third group of of uning electry of digital termi- ce various folds of engineering unication, meadlungs, else are di m and vice versa as well as proble | gs to quick responde. The second g synthesis of pulse systems with real pulse someoness, to the stuff of systems, and to the nethods of each pulse systems are business. | a Problems of Theory and Application in Money from Springer 22 to do to classuasions of the present six to classuasions and to planning for at the conference have been divide at the conference have been divide the total partial are discuss marticular point ing control system menticular point in the control s | anders. | , Deter of "e-initeal Sciences, Nu. T.A. Kickel Littor, Candidate of Ti miteal Sciences, 1.5. Krimamov (Sci haiteal Sciences, 1.5. Rel domur, De lichte of Technical Sciences, and N. House: N.I. Podgystakij; Tech. House: N.I. Podgystakij; Tech. | sub SISR. Mataional'nyy komitet Si tut aviomatiki i telemekhaniki. | h artomaticheskikh sistem; trudy k teorete Automatic Systems; Transact 1, 1993, 572 p. 5,000 copies prin 1, 1993, 572 p. 5,000 copies prin | i primeneniya diskretnyth svicmat | SE I BOOK EXPLOITATION | |
| the state of the s | ! | | in an Opti- 1 with solving es the Galerkin | | | alizing control alizing control areations made dur- lean included in t of the papers. | cateal applications cateal systems, are also found conditions in | payers naul de varia fine and de introdu less, provir engi- sciased. Problema a of developing | rony of papers is ribble paresetars, f self-outlibrach follating librair ightens of semy | 1938. It was the of the theory ing of the theory if into four groups ed as well as methods eas in which are | ODITOTORICO ALLA | w Dolcalence, two Dolcales, contain Schanzer, contific Secretary), cotor of Technical 1.2. tarpkin, cot Technical 1.2. tarpkin, cot Technical 1.3. S.G. Markowich. | St be antomers. | ongermous stone tol. | loheskikh sistem, | 201/1711 | |

| Exits, s.G. (Noseror). Optimalising Systems of Turbine Drilling With Discrete Myriss problem consists of astabilishing a maximum drilling speed for a given last on the chisely, its technological conditions, and a given arrains. The author describes a structural scheme of the optimalising control system for a turbine drilling installation. There are no references. Laskerich, Lie, Lie, Lorallow, and E.G. Existationer. Electronic Optimalising Controlling arrains and give a detailed description of the peak-holding deciral seasted of optimalising control. There are 7 references: 5 Structs of the peak-holding it renclation) and 2 Explish. | test of automatic Optimisation of automatic Single-Action Minister in Discrete Systems of automatic Optimisation The author defines the problem of automatic optimization as the process of extendishing a minister value for a certain input quantity E through subcurse title seaming. This process is a single-ection one and the schools used are the same as those discreted in the paper delivered by R.I. Statherskiy (p.905). The surface considers the method of the quincest triggering as the most economical. Se describes the practicable equipment for developing this type of eutratic ministers. | | purposit: These transactions are intended for the numbers of the sociations and principal to the sociations and intended control. COTENIAN: The Conference on the Problems of Theory and Application of Discrete antended Systems took place in Newton from Systems 22 to 26, 1958. It was an examine Systems and the planeth state of the theory the first conference automatic systems and to planning for fature development. The papers discussed as the conference have been discussed as veil as swholes in the first group optimisation soliching strends are been discussed as veil as swholes for relay control systems, in particular plant ing control systems and which are realized systems presents as to quick response. The sound system with swretch parameters, developed to the activity and systems of submitting points systems with swretche parameters, of place options in solicitude principal constitution placements in such taken place systems, and to the activity of self-controllation place systems with swretch systems, and to the activity of self-controllation placements in such taken place systems, and to the activity of controllation place systems with swretch self-controllation placements in such taken place systems, and to the activity of controllation placements in such taken place systems, and to the activity of controllation place systems with swretches place systems with swretches and to with the such controllation of such placements. | | Honerentein po woprozem tworii i primeneniya diskretoyth evtomatichenkikh sistem, 1928 Noscaw, 1928 Teorlym i primenenty diskretoyth ertomatichenkikh sistem; trudy konferentell (Theory and Application of Discrete Automatic Systems; francetions of the Conference) itemory, 18 SANN, 1900, 572 p. 3,000 contemporation or treatments. | FBLER 1 BOOK ENTROPERS 507/411 |
|---|---|--|---|--|---|--------------------------------|
|---|---|--|---|--|---|--------------------------------|

16,4000 (1121,1132,1013)

28368 S/124/61/000/008/006/042 A001/A101

AUTHOR:

Kazakevich, V.V.

TITLE:

On the process of extremum controlling of inertial objects at the presence of disturbances

PERIODICAL: Referativnyy zhurnal. Mekhanika, no. 8, 1961, 13, abstract 8A123 (Mezhdunar. federatsiya po avtomat. upr. I Mezhdunar. kongress po avtomat. upr., Moscow, AN SSSR, 1960, 19 pp, ill.)

TEXT: The author considers a method of reducing the effect of inertness of an object on the process of experimental step regulation. Inertness of an object is described by a linear differential operator with an extremal function in the right-hand side. The method consists in the discrete measuring of the output magnitude of the object or its derivatives within the "step" of regulation and in the forecasting of the steady value of the output magnitude for the given step. The forecasting of the steady value is conducted on the basis of the form of the solution of the linear differential equation and the results of discrete measurements of the output magnitude, without allowance for random errors of these measurements.

[Abstracter's note: Complete translation] Card 1/1

A. Krasovskiy

/6,8000 (1121,1132,1344)
AUTHOR: Kazakewich, V. V.

s/044/61/000/005/022/025 0111/0444

AUTHOR:

TITLE:

A study of non-linear processes in an extremal control

PERIODICAL:

Referativnyy zhurnal, Matematika, no. 5, 1961, 27, abstract 5V181. ("Teoriya i primineniye diskretn. actomat. sistem." M., ANSSSR, 1960, 387 - 398)

The Galerkin method is applied to the study of extremal TEXT: controls, which is connected with the solution of systems of non-linear ordinary differential equations. For systems the object of which is described by a linear differential equation of first or second or-

der, the author uses the following solution set-up: $y = b + \sum_{i=1}^{\infty} (A_i \sin i\omega x + B_i \cos i\omega x)$

for systems with non linear objects, he uses the set-up:

 $y = b - \Delta_1 \sin^2(\omega x + \varphi)$.

Various special cases are considered. Graphical representations of the Card 1/2

26159 8/044/61/000/005/022/025 0111/0444

A study of non-linear processes...

solutions are given.
(Abstracter's note: Complete translation.)

Card 2/2

33568 S/194/61/000/012/052/097 D256/D303

26.2120

Bodner, V. A. amd Kazakewich, V. V.

TITLE:

AUTHORS:

Self-oscillations of acoustical systems containing compressors and their suppression using feedback sys-

tems

PERIODICAL:

Referativnyy zhurnal, Avtomatika i radioelektronika, no. 12, 1961; 53, abstract 12V473 (Avtomat. upr. i vychisl. tekhn. no. 3, M., Mashgiz, 1960, 445-490)

TEXT: Self-oscillations of air pressure and the rate of flow in ventilators, compressors and turbo-jet engines (pumps) render their operation more difficult or in certain circumstances even impossible. The oscillation frequency and intensity depend upon the following factors: The characteristics of the compressor, the length and shape of the inlet and outlet tubes, the acoustic load at the end of the tubes and the steady flow parameters. A theory of the compression processes is presented, considering the compressor with the attached network as an acoustical distribution system by Card 1/3

APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000721230005-1"

33568 S/194/61/000/012/052/097 D256/D303

Self-oscillations of ...

substituting an equivalent active non-linear resistance for the compressor, acoustical distribution systems for the tubes and localized resistances for volumes and chokes. Assuming a small increase of the parameters of flow, the equations of hydrodynamics and the state equations are reduced to a linear form corresponding to a wave equation including dissipation forces. The non-linearity of the compressor characteristic can be included in the boundary conditions. The solution of the quadrupole wave equation is obtain , ned by Fourier's method. It contains the dimensionless complex frequencies, whose real part represents the frequency of the oscillations and the imaginary part - the logarithmic decrement of attenuation characterizing the stability of the system. The stability was investigated for a system containing one outlet tube loaded with an arbitrary acoustical resistance. The phase-plane of the system was established, and from it the regions of static and dynamic stability as well as instability were determined. A similar investigation was carried out for a compressor with a single inlet tube, and also for a combination of both the inlet and outlet tu-

Card 2/3

33568 S/194/61/000/012/052/097 D256/D303

Self-oscillations of ...

bes present. It was found in particular that the resistance distributed in the tubes connected to the compressor increases the surplus stability of the compressor. There are 10 references. / Abstractor's note: Complete translation. /

X

Card 3/3

S/103/60/021/04/04/007 B014/B014

AUTHOR:

Kazakevich, Y. Y. (Moscow)

TITLE:

Theory of the Ideal Model of an Extremal Controller

PERIODICAL: Avtomatika i telemekhanika, 1960, Vol. 21, No. 4, pp. 489-505

TEXT: Automatic control systems frequently have to keep the quantity to be controlled at an extreme value or to prevent this quantity from exceeding a certain value. In the present paper, the author analyzes the mode of operation of an extremal controller using the methods of point transformation. The mode of operation is explained by means of the schematical representation shown in Fig. 1, after which the control processes are described. It is assumed that p = f(v) for the quantity to be controlled. Here, v is a parameter. Then, a point v^* of v is defined, which is invariant with respect to a T-transformation. This point is calculated from the equation (B) $\delta = f(v^*) - f(v^* - \Delta v/2)$. The nature of the control process and the number of invariant points satisfying (B) are thoroughly studied in an extensive investigation. Among other things, it is shown that there is only one point on the ray $v < v^*$ that remains

Card 1/3

Theory of the Ideal Model of an Extremal Controller

S/103/60/021/04/04/007 B014/B014

invariant in T-transformation, namely, v*. Furthermore, the positions of individual points v_1 , v_2 ,... after the transformation are examined and, thus, the nature of the control process is disclosed. A study of the effect of changes in the parameters $\triangle v$ and δ upon the nature of the control process shows that an increase of $\triangle v$ has the same effect as a

decrease of δ . Assuming that $p = -v^2$ (27) holds for the relation p = f(v) the author studies a practical example. The possible motions of the system depend on the two parameters Δv and δ . The modes of control are graphically represented (Fig. 2) in the plane of the parameters Δv and δ . For $\Delta v = 3$ and $\delta = 1$ Fig. 3 shows a "phase diagram" of control to which range 1 corresponds in Fig. 2. The course of control in time is shown in Fig. 4 for the same case, for $\Delta v = 2$, and for $\delta = 1$. A comparison of the two curves indicates that the first case of control is less convenient than the second case, due to its longer control period and its higher control amplitude. It is finally shown that the accuracy of control is much more affected by a decrease of Δv than by an increase of δ . The article under review was first published in Trudy TSIAM in 1949, and the present copy is an exact reprint.

Card 2/3

Theory of the Ideal Model of an Extremal Controller

S/103/60/021/04/04/007 B014/B014

There are 6 figures and 2 Soviet references.

SUBMITTED: July 6, 1959

Card 3/3

27639 S/194/61/000/002/028/039 D216/D302

16.8000 (1013, 1068, 3005)

AUTHORS: Kazakevich,

Kazakevich, V.V, Kornilov, R.V. and Khristoforov,

N.G.

TITLE:

Electronic extremum controller

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 2, 1961, 39, abstract 2 V316 (V sb. Teoriya i primeneniye diskretn. avtomat. sistem, M., AN SSSR,

1960, 558-569)

TEXT: In an extremum controller operating with storage of the extremum, the fundamental disturbance is the fast monotonically disappearing extremum characteristic. For the stabilization of the position of the controlling device it becomes then advantageous to use a commutator which periodically reverses the speed of the machine. The presence of inertia or delay in the load influences the steady-state of a system with such a controller. If in a load without inertia in its steady-state positive and negative increments

Card 1/2

27639 S/194/61/000/002/028/039 D216/D302

Electronic extremum controller

alternate, then in the load with inertia after a few positive increments, the same number of negative increments will follow (the characteristic is said to be symmetrical). The bloc-diagram of extremum controller consists of a signum-relay determining the sign of the increment, a commutator and output device. The operation of the signum-relay and of the commutator are synchronized. The extremum controller has been tried on a model of the load. 7 references.

Card 2/2

s/020/60/133/04/03/031 B019/B060

13, 2000

AUTHOR:

On the Extreme Regulation of Inertial and Unstable

TITLE Objects

Doklady Akademii nauk SSSR, 1960, Vol. 133, No. 4, PERIODICAL:

pp. 756-759

TEXT: The author studied the system for the extreme regulation shown in Fig. 1, which consists of an inertial member, a nonlinear element, a device for the formation of signals, a signum relay, and a slave. This system exhibits an extremal dependence of the output signal of the inertial member on the input signal x of the nonlinear element; here, therefore, the inertia acts after the nonlinear element. The problem of extreme regulation consists in finding and maintaining y on the maximal value as a function y = f(x). After pointing to the difference between the dynamic and the static value of the quantity y, caused by the inertial member, the author considers a procedure for the extreme regulation, by which it is possible to eliminate completely the influence of Card 1/3

On the Extreme Regulation of Inertial and Unstable Objects

82514 s/020/60/133/04/03/031 B019/B060

inertia on the searching time, and by which it is possible to get rid of the unfavorable influence of low-frequency external disturbances. The differential equations (1) and (1!) linking y to x are written down, and it is shown in a general study of these equations that the finding of the extreme is the more precise the larger the cross bar velocity. With the existence of an inertial object losses arise during the searching and so do larger oscillation amplitudes. A drawback exhibited by the method described here due to an insensitivity zone of the signum field is then discussed along with the ways of avoiding it. The positive aspects of the method are dealt with next. It is found in this connection that the system for extreme regulation, dealt with here, functions even with a very steep form of the extreme dependence and with very slow shifts of the extreme. Moreover, the approach to the extreme point is quick, and the influence of the external low-frequency disturbances is excluded. This method can be also used for the regulation of neutral and unstable systems. The extremal regulation of undamped oscillating objects and of unstable objects is finally dealt with, and the problem is discussed, as to how the searching time can be reduced, if an inertial member acts as far as the extreme element. A. P. Yurkevich is mentioned. There are

Card 2/3

S/020/60/133/005/002/019 B019/B054

AUTHOR:

Kazakevich V. V.

TITLE:

On the Reduction of the Influence of Inertia in Extreme-

value Control of Objects of the n-th Order

PERIODICAL:

Doklady Akademii nauk SSSR, 1960, Vol. 133, No. 5,

pp. 1041 - 1044

TEXT: It is assumed for this investigation that the regulator under review is working according to the "storage of maximum" principle, from which it follows that the reversion of the final control organ, i.e. the change of the sign of the velocity x at the input of the object, takes place after the dynamic quantity y of the object output, measured by a sensitive element, has passed through a maximum. In the case of an inert object, there is a difference between the dynamic curve y and the static curve y*, and the scanning rate can be reduced by reducing this difference. Another possibility of reducing the inertia of the object is to find a method of establishing, within a finite time, the value y = y* which, in

Card 1/2

APPROVED FOR RELEASE: 06/13/2000

CIA-RDP86-00513R000721230005-1"

S/020/61/136/004/005/026 B019/B056

16,9500 (1031,1121,1132)

AUTHORS: Kazakevich, V. V. and Yurkevich, A. P.

TITLE: Improvement of the Extremum Control of Inert Objects in the

Presence of Disturbances

PERIODICAL: Doklady Akademii nauk SSSR, 1961, Vol. 136, No. 4,

pp. 783 - 786

TEXT: In a previous paper (Ref.2), V. V. Kazakevich described a method for extremum control, which permits avoiding the action of the inertia of the object in the absence of dynamic terms in the object. In this system, a certain combination of signals is fed to the input according to the a certain combination of signals is fed to the input according to the derivative of the quantity to be regulated. In the case of objects with low-frequency disturbances, this system offers special advantages, as the disturbances are filtered out. However, in the case of considerable disturbances, a considerably varying level of the extremum of the function, and, in the case of moderately fast cross beams of the final control organ, scarning may be considerably disturbed. The authors first confine themselves to control systems of first-order objects; the extremum element

Card 1/4

APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000721230005-1"

Improvement of the Extremum Control of Inert S/020/61/136/004/005/026 Objects in the Presence of Disturbances B019/B056

is characterized by the relation $y_1 = -K_x^2$ (1) is assumed, where x and y_1 are the input and output coordinates of the extremum element. It is further assumed that $|\dot{x}| = V_x = \text{const}$, and that between the inputs of the objects y_1 and y_2 the relation $y_2 = k_0 y_1/(p\tau_0 + 1)$ holds, where k_0 and τ_0 are constants. In the control method developed in Ref.2, the signal $z = K_D \dot{y}_2$ is fed to the input of the extremum regulator if nonlinear terms are not taken into account; in this case, the following relation holds with $y_1 K_D K_0 / \tau = y$: $z = p\tau_0 y/(p\tau_0 + 1)$ (3). The symbols used here have been taken from Ref.2 and are not defined more closely. The transition processes in the system investigated here are described by a system of equations that is analogous to that describing the transition processes in an inertialess object with a dynamic input signal converter. Such systems have already been studied by A. P. Yurkevich (Refs. 3,4). Some results of these investigations are discussed, and, following this, it is assumed that the external disturbances are a linear function of time. (1) is then replaced by $y_1 = -K_x x^2 + K_1 t$ (4). As may be seen from a graphical

Card 2/4

Improvement of the Extremum Control of Inert S/020/61/136/004/005/026 Objects in the Presence of Disturbances B019/B056

representation of the control process, an oscillation with decreasing amplitude occurs near the extremum, the amplitude approaching a limit. Considerable disturbances are then briefly dealt with, which are a quadratic function of time. It is shown that in this case considerable deviations may occur, and it is noted that by a decrease of time, in the case of both linear and quadratic disturbances, the transition process may, in general, be shortened, and the amplitude may be decreased. It is then shown that by using a combined converter system for the input signal, the quality of extremum control is improved. The dynamic converter, in the case of an optimum time constant, suppresses the undesired influence of low-frequency disturbances, and the negative feedback of the insensitive range increases the accuracy of control near the extremum during the action of monotonic external disturbances. For the purpose of determining the parameters of the transition processes and of the limit cycles of the system, the construction of phase trajectories in multi-folium surfaces is of advantage. For an ideal case, in which instrument errors are excluded and the action of the inertia of the object may be neglected, the construction of phase trajectories is discussed in detail. There are 3 figures and 6 Soviet references.

Card 3/4

Improvement of the Extremum Control of Inert S/020/61/136/004/005/026 Objects in the Presence of Disturbances B019/B056

ASSÖCIATION: Moskovskiy aviatsionnyy institut im. Sergo Ordzhonikidze (Moscow Aviation Institute imeni Sergo Ordzhonikidze)

PRESENTED: July 26, 1960, by N. N. Bogolyubov, Academician

SUBMITTED: July 12, 1960

Card 4/4

13,2000

S/569/61/002/000/006/008 D298/D302

AUTHOR:

Kazakevich. V.V. (USSR)

TITLE:

On extremum control of plants with lag and

disturbances

SOURCE:

IFAC, 1st Congress, Moscow 1960. Teoriya diskretnykh,

optimal'nykh i samonastraivayushchikhsya sistem.

Trudy, v. 2, 1961, 791 - 816

TEXT: Methods are considered for compensation of lag and of disturbances. First, a method is considered which would speed up the search process by 50 - 100 times. It is assumed that the extremum controller operates by the principle of storage of maximum. The cscillatory nature and inaccuracy of the process will be the smaller, the nearer the dynamical—and statical curves y and y*. This can be achieved by reducing the search time. This method however involves a large increase in settling time. Another way for lag compensation, is the following. It is necessary to find a method of search, in finite time, for the value y₀ = y*, which the actual Card 1/11

S/569/61/002/000/006/008 D298/D302

On extremum control of plants ...

system attains after an infinite time-tapse. This problem cannot be solved for every type of function f(x) if the input x is continuous as thereby the velocity of y is determined by the unknown function f[x(t)]. For step systems, the problem is solvable. A first-order object (plant) of type

 $T\hat{y} + y = f(x) \tag{1}$

is considered, where y is the output variable, x - the input variable and T - the time constant. The transient process in the step system is described by

$$T_1 \overline{y}_1 + \overline{y}_1 = f(x_1) - f(x_0) = a_1,$$
 (4)

where $\bar{y}_1 = y - y_0^*$. The solution of this equation is

$$\bar{y}_1 = a_1(1 - e^{-\frac{t}{T_1}})$$
 (5)

Card 2/11

X

On extremum control of plants ...

S/569/61/002/000/006/008 D298/D302

or
$$y = y_0^* + [f(x_1) - f(x_0)](1 - e^{-\frac{t}{T_1}}).$$
 (5a)

If t approaches infinity, then e^{-t/T_1} approaches zero and $\bar{y}_{\infty} = a_1$,

$$y_{\infty}(x_1) = y_1^* = y_0^* + [f(x_1) - f(x_0)] = y_0^* + a_1^*$$
 (6)

By means of Eqs. (5) and (6), it is possible to determine (in a finite period) the value a_1 which the actual system attains after an infinite time. For this purpose it is necessary to set, after the input x has been given the increment \triangle , two time-delays and to measure the values of \bar{y}_1 at the end of these intervals. Let the time delays be denoted by π . A system of two equations with two unknowns is obtained, whose solution is

$$a_1 = \frac{\bar{y}_{11}^2}{2\bar{y}_{11} - \bar{y}_{12}};$$
 (8a)

Card 3/11

30560 S/569/61/002/000/006/008

On extremum control of plants ...

$$T_1 = -\frac{\tau}{\ln(\frac{\bar{y}_{12}}{\bar{y}_{11}} - 1)}$$
 (8b)

Thereupon, the input x is again displaced by \triangle , and a₂ and T₂ are obtained. Two consecutive values of y_2^* and y_1^* are introduced into the signum-relay and the difference

$$\delta_1 = y_2^* - y_1^* = (y - \bar{y}_{12} + a_2) - (y_0^* + a_1) = \bar{y}_{12} + (a_2 - a_1)$$

is found. For the n-th cycle one obtains:

$$\delta_{n} = \overline{y}_{n2} + (a_{n+1} - a_{n}).$$

Hence it follows that it is not necessary to store and to add all the \bar{y}_{12} and a_i . If the controller has, in addition to a device which measures the output variable y, a tachometer for measuring derivative \hat{y} , then a single time-delay only, is necessary. Ascard 4/11

30569 S/569/61/002/000/006/008 D298/D302

On extremum control of plants ...

sume the plant is linear and its time constant T_1 is known; in this case a can be found if a pair of values y_1 and $t_1 = \tau$ are known which satisfy Eq. (5). As before, the difference δ_n is obtained after n cylces:

$$\delta_{n} = y_{n+1}^{*} - y_{n}^{*} = k\overline{y}_{n+1} - (k-1)\overline{y}_{n1}.$$

The above argument can be extended to a plant which is described by an n-th order system of differential equations with constant coefficients:

$$y^{(n)} + b_1 y_1^{(n-1)} + \cdots + b_n y = 0.$$
 (17)

It is assumed that the properties of the plant are known, hence all the roots λ of the characteristic equation are known. The solution of the equation which describes the transient process is

$$\bar{y}_1 = \frac{a_1}{b_n} + \sum_{k=1}^{n} A_{k1} e^{-\lambda_k t}$$
 (22)

Card 5/11

On extremum control of plants ...

S/569/61/002/000/006/008 D298/D302

For t = co,

$$\overline{y}_{1\infty} = \frac{a_1}{b_n} . \tag{24}$$

The quantity \bar{y}_{100} is determined by the same method as before, i.e. \bar{y} is measured at the end of several time-delays (intervals). As a result one obtains a system of (n+1) equations in (n+1) unknowns. Calculating the quantity a_1/b_n by means of a computer, the steady-state value of y_1^* is found. Then y_2^* is determined, and δ_1 :

$$\delta_1 = y_2^* - y_1^* = (y_0 + \overline{y}_{1,n+1} + \frac{a_2}{b_n}) - (y_0 + \frac{a_1}{b_n}).$$

The measuring process continuous as above. In the case of one measuring device, (n+1) time-delays are necessary. With increasing number of measuring devices, the number of time-delays decreases correspondingly. Thus, if measuring devices for the output varia-

Card 6/11

Y

On extremum control of plants ...

8/569/61/002/000/006/008

ble and for the first (n-1) derivatives are used, only a single time-delay is necessary. If the process is aperiodic and the roots λ are unknown, the number of unknown variables increases to 2n+1. In this case 2 time delays are necessary if the output and the (n--1) derivatives are measured. If the velocity of the external disturbances can be considered as constant over the total time-delays then it is possible to compensate the disturbances by increasing the number of delays τ by one. Two cases are considered: 1) A first-order plant with lag, and 2) Without lag. In the first case, a system of 3 equations with the 3 unknowns y_1^2 , b_1 and T_1 is obtained (b_1 denotes the constant velocity of the disturbance and T_1 the lag). Depending on the sign of $\delta = y_{i+1}^* - (y_i^* + 3\tau b_i),$

the signum-relay changes the direction of the input. Then the next step of the search process starts (with y_{1+2}^*), etc. Further, the character of the transient processes at each of the stages is considered. In case of a plant without lag (T = 0), only 2 equations Card 7/11

On extremum control of plants ...

S/569/61/002/000/006/008 D298/D302

are required. A plant with nonlinear dynamical elements is described by

$$\Psi_1(y', y'', ..., y^{(n)}) + \Psi_2(y) = f[x(t)]$$
 (51)

where

$$\hat{\psi}_1 = y^{(n)} + \psi_{11}(y', y'', \dots, y^{(n-1)}).$$

Eq. (31) is written in the form

$$\psi_1(y', y'', \dots, y^{(n)}) = f(x) - \psi_2(y).$$
 (33)

It is necessary to find the static ("potential") maximum of y. This can be attained if the right-hand side of Eq. (51) is a maximum. From Eq. (33) it is evident that with $\Psi_2(y) = \text{const.}$, the maximum of f(x) will correspond to the maximum of Ψ_1 . Thus, by introducing the function Ψ_1 in the extremum controller and by searching for its maximum at sufficient speed of the controller, this maximum will be attained for a value of $x \approx x^*$ which maximizes the function f(x); with such a value of x^* , the variable y assumes maximum Card 8/11

On extremum control of plants ...

S/569/61/002/000/006/008 D298/D302

value too, (after the transient processes in the lag element have ceased). This result is valid if y = const., which is the case with inifnite speed of search. In practice however, this speed is limited; nevertheless, if the speed is sufficiently high, the search for ψ_{lmax} approximates the search for $r(x)_{max}$. Thereby the low-frequency disturbances do not affect the search process. It is noted that, unlike ordinary extremum-systems, the extremum-search under consideration will the more accurate, the nigher the speed of computation. The above method of extremum control has the foilowing advantages: 1) The control system will operate even if the form of the extremum functional-dependence is very smooth. 2) The extremum point is approached with maximum speed and little munting; low frequency disturbances are compensated. 5) The method is also applicable to neutral- and unstable systems, and to systems with modulated input. Further, a variant of the method is considered, which yields a solution to the problem, with any speed of computation. Hitnerto, it was assumed that the lag element rollows the extremum controller; if there is also a lag element preceding the controller, the search process can be speeded up by changing the position of the controller. It is noted that the step-wise method Card 9/11

30566 S/569/61/002/000/006/008 D298/D302

On extremum control of plants ...

(of the first section of the report) is more advantageous whenever the time constants of the plant have to be determined during the process which is the case with systems of order higher than the first. In the case of white noise or high-frequency noise components, the likelihood that signal and noise will coincide, can be reduced by alternating the frequency of the signal. In the case of a plant with lag, random noises and constant disturbances, the hunting can be reduced by a combination of the above methods. A figure shows the block-diagram of a setup which operates by the combined method. This setup incorporates a "guarding" device which stops the search if the extremum is attained and renews it if the controlled variable deviates from the extremum by a given value. A discussion followed. Taking part were: A.P. Yurkevich, V.P. Putsillo, Yu.I. Ostrovskiy, A.A. Pervozvanskiy, I.S. Ukolov (USSk). There are 7 figures and 8 references: 6 Soviet-bloc and 2 non-Soviet-bloc. The references to the English-language publications read as follows: S. Serdengecti, Optimalizing control in the presence of noise interference. Jet. propulsion, v. 26, no. 6, 1956; G. Vasu, Experiments with optimalizing controls applied to rapid

Card 10/11

X

30560 S/569/61/002/000/006/008 D298/D302

On extremum control of plants ...

control of engine pressure with high-amplitude noise signals. Trans. ASME, v. 79, no. 3, 1957

Card 11/11

X

APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000721230005-1"

24.4100

h1277 \$/588/62/000/005/004/004 I011/1242

AUTHOR:

Kazakovich, V.V.

TITLE:

The approximate investigation of some types of strongly

non-linear autonomous systems

SOURCE:

Avtomaticheskove upravlenive i vychislitel'naya tekhnika.

no. 5. Moscow, 1962, 365-442

TEXT: A second-order system described by

 $\ddot{x} + k^2 x + \mu f_1(x, \dot{x}) = 0$

(1)

is investigated. The method proposed here is independent of the magnitude of μ and yields very good results when investigating non-linear conservative systems if the elastic force increases monotonically with the deviation while its x derivative decreases monotonically. The method can be applied to many non-conservative systems, especially when the oscillation period is determined. It is possible to establish how nearly a given system approaches any linear system. The shortcomings of Van der Pol's method are pointed out;

Card 1/3

S/588/62/000/005/004/004 IO11/T242

The approximate investigation of ...

since the method is based on averaging over a period, it cannot bring cut the effect of friction forces in dissipative systems which are symmetric about the origin. This brings forth the idea of breaking up the given system, in which the character of cooperation between the friction and the elastic forces changes several times in a given period, into as many "quasi-conservative" systems. The character of this cooperation will be constant in each of these systems and will equal that in the corresponding part of the cycle in the original system. The solution of each system coincides with the solution of the given system in the corresponding part of the cycle. Some possible cases are investigated: (a) symmetry of the phase diagram about both coordinate axes; (b) no symmetry of the integral curves about the coordinate axes; (c) dissipative systems; (d) self-oscillating systems; (e) symmetry about the abscissa; (f) symmetry about the ordinate; (g) non-symmetric system. A method of finding the form of oscillations is given. Its use is illustrated in an example. A method for an approximate integration

Card 2/3

APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000721230005-1"

S/588/62/000/005/004/004 I011/1242

The approximate investigation of ...

of systems with one degree of freedom is proposed an applied. Results are compared with those of other methods. The deviation of the results from those of the small-parameter methods is a measure of the amount by which the given system approaches a linear one. The method described here is applied to higher-order systems. There are 23 figures and 3 tables. The most important English-language reference is: B. Van der Pol, Radio Review, 1, p.701, 1920, Phylos. mag. 7,2, p. 978, 1926.

Card 3/3

KAZAKEVICH, V.V.

Approximate study of some types of strongly nonlinear autonomous systems. Avtom. upr. i vych. tekh. no.5:365-442 162.

(MIRA 15:9)

(Automatic control)

KAZAKEVICH, V.V., prof., doktor tekhn. nauk; PASHKOVA, V.N., red.

[Automatic control of technological operations] Avtomaticheskoe regulirovanie tekhnologicheskikh protsessov; uchebnoe posobie po kursu "Avtomaticheskoe upravlenie i regulirovanie tekhnologicheskikh protsessov v poligrafii." Moskva, Mosk poligr. in-t, 1963. 65 p. (MIRA 16:9)

(Automatic control)
(Printing machinery and supplies)

KAZAKEVICH, V.V. (Moskva); OSTROVSKIY, G.M. (Moskva)

Problem concerning indirect control taking into account coulomb friction in the sensitive element. Avtom. 1 telem. 24 no.8:1141-1144 Ag '63. (MIRA 16:8)

(Automatic control)

MAZAKEVICH, V.V.

Optimulizing control. Avicm. upr. i vyen. tekh. no.6:7-5) 162.

(MIRA 17830)

jw

Cord 1/1

SUB CODE:

UDC:

621.3.078

LIBERZ'N, Leonid Mikhaylovich; RODOV, Aleksandr Borisovich; KAZAKEVICH, V.V., prof., red.; POFKOV, Yu.S., red.

[Optimalizing control systems] Sistemy ekstremal'nogo regulirovaniia. Pod red. V.V.Kazakevicha. Moskva, Energiia, 1965. 158 p. (Biblioteka po avtomatike, no.154) (MIRA 19:1)

 $L^{1}8344-66$ EEC(k)-2/EWA(h)/EWP(k)/EWT(d)/EWT(1)/EWP(v)/EWP(l)/EWP(h) SOURCE CODE: UR/0286/65/000/018/0097/0098 AP5025750 CIA-RDP86-00513R000721230005-1 ORG: none TITLE: Past acting meumatic regulator. Class 42, No. 174866 SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 18, 1965, 97-98 TOPIC TAGS: pneumatic regulator, automatic control, PNEUMATIC CONTROL, CONTROL SYSTEM ABSTRACT: This Author Certificate presents a fast acting pneumatic regulator based on DSEPPA elements containing a first derivative transducer, a signum-relay, a checking reverser commutator, a reverse trigger, and an actuating mechanism. To increase the regulator stability margin during drifting of an extreme characteristic, the signumrelay output is simultaneously connected to the inlet of a blocking relay and through a discrete memory element to the inlet of an intermediate relay. The latter is connected to the blocking relay, and its outlest is connected to the reverser trigger. 13/ SUBM DATE: SUB CODE:

AND THE PROPERTY OF THE PROPER

| L 09269-67 EWT(d)/EWP(v)/EWP(k)/EWP(h)/EWP(l) ACC NR. AP6029887 (A) SOURCE CODE: UR/0413/66/000/015/0049/0049 3.2 |
|---|
| INVENTOR: Kazakevich, V. V. |
| OriG: none |
| TITLE: Method for extremal control of objects whose motion is described by an n-th order differential equation. Class 21, No. 184317 |
| SOURCE: , Izobret prom obraz tov zn, no. 15, 1966, 49 |
| TOPIC TAGS: optimal control, control circuit |
| ABSTRACT: This Author Certificate presents s. method for extremal control of objects whose motion is described by an n-th order differential equation. To simplify whose motion of the optimum with fast continuous variation of the controlling parameter, location of the optimum with fast continuous variation of the controlling parameter the moment of passage through a zero of the n+l-st derivative of the output parameter the moment of passage through a zero of the n+l-st derivative of the output parameter is varied with is recorded and the direction of motion of the controlling parameter is varied with the variation of sign of this derivative (see Fig. 1). |
| Fig. 1. 1 - dynamic element; 2 - nonlinear, (extremal) element; 3 - differentiating device; 4 - trigger; 5 - control element |
| Orig. art. has: 1 diagram. Cord 1/1 SUB CODE: 29 SUBM DATE: 04May60 UDC: 621.3.078 |

extremum characteristics and make it possible to determine the extremum value of the input in the minimum time and with the smallest "yawing" of the input coordinate. The derived algorithm for climinating the inertial effect

Cord 1/2 UDC: 62-50
APPROVED FOR RELEASE: 06/13/2000 CI

000 CIA-RDP86-00513R000721230005-1"

| ACC I | The der | nded to pen with the rived als ent of the take in the rives and the rives are rives are rives and the rives are ri | e input | r search t every t the h | hino the | 6 STriem | 734 | | - deter | toline | |
|-------|---------|--|----------|--------------------------------|--|----------|-------|--------|-----------|--------|--|
| | 4 figu | g and | DATE: 04 | Jan66/ | ORIG RI | SF1 007 | / ATD | PRESS: | 5112 | • | |
| SUB | CODE: | M EARW | DVID! O. | . 1 | | | | | | | |
| | | | | | | | | | + 4 1 1 1 | | |
| | | | | | $: \mathbb{R}^{n}$ | | | • | • 1 | | |
| | | | | | | | | | | | |
| | • | | | | | • • • | | | * | | |
| 1 | | 1 | | | | | | * | | | |
| | | | | | | | • | * | | | |
| | | | | | To the second of | | | 10 T 1 | | | |
| | | | · April | • | | | | | | | |
| - 1 | | | | | | | | | | | |

